

Episode 13

Free Vibration of Damped Systems

ENGN0040: Dynamics and Vibrations
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Topics for today's class

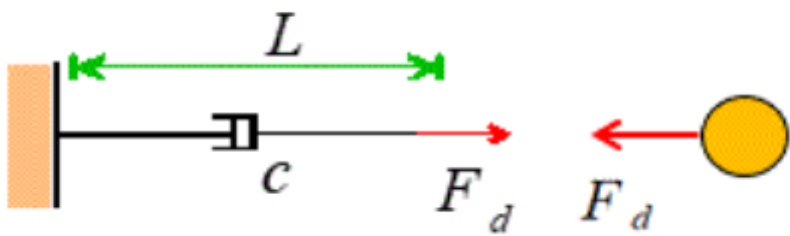
Free Vibration of Damped Systems

1. Modeling energy dissipation – the dashpot
2. Damped harmonic oscillator
3. Terminology
4. Examples
5. Measuring damping experimentally

5.5 Free Vibration of damped systems

Goal: Understand influence of energy loss on free vibrations

5.5.1 Modeling energy loss: The dashpot



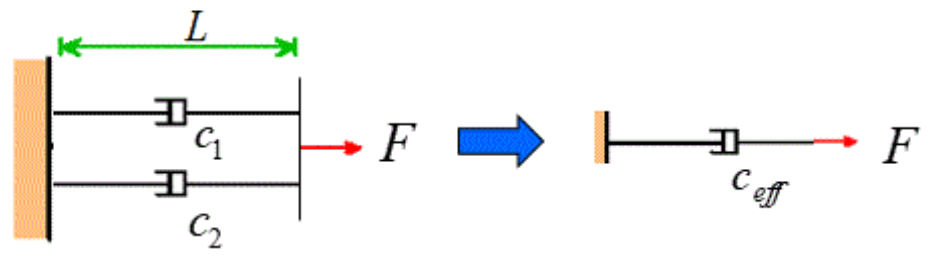
Exerts a force proportional to stretch rate

$$F_d = c \frac{dL}{dt}$$

c : "Dashpot coefficient"
(constant - similar to spring stiffness)

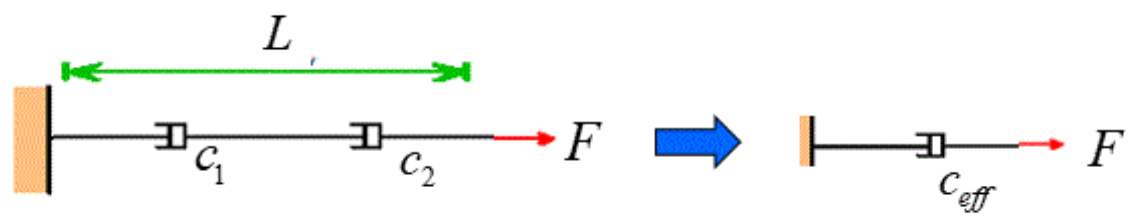
Units Ns/m

Can combine like springs



Parallel

$$C_{eff} = C_1 + C_2$$

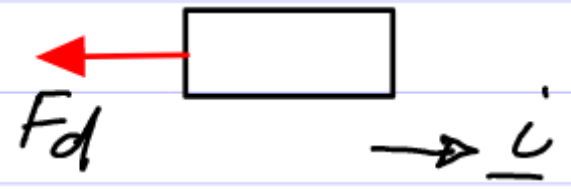


Series

$$\frac{1}{C_{eff}} = \frac{1}{C_1} + \frac{1}{C_2}$$

Power to stretch a dashpot

$$P = \underline{F} \cdot \underline{v} = -c \frac{dL}{dt} \underline{i} \cdot \frac{dL}{dt} \underline{i}$$

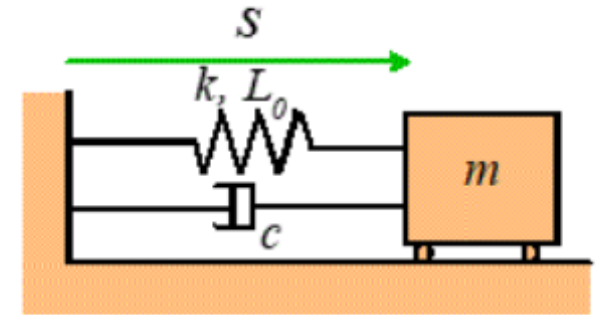


$$P = -c \left(\frac{dL}{dt} \right)^2$$

Always < 0
 $\Rightarrow$ always dissipates energy

5.5.2 Free Vibration of a 1-DOF system

Canonical vibration problem: The spring-mass system is released with speed v_0 from position s_0 at time $t=0$. Find $s(t)$



Approach : (1) EOM
(2) Find solution in tables

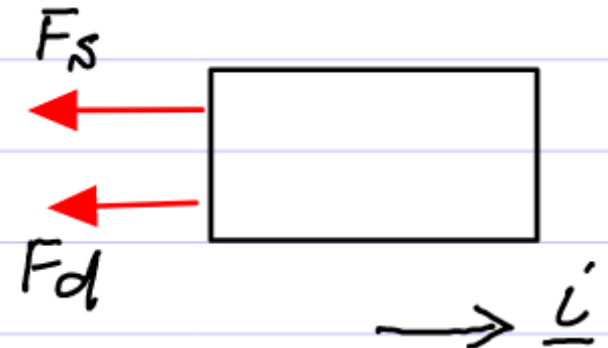
EOM ($F = ma$)

$$-F_s - F_d = m \frac{d^2 s}{dt^2}$$

$$F_s = k(s - L_0) \quad F_d = c ds/dt$$

$$-k(s - L_0) - c ds/dt = m d^2 s / dt^2$$

$$\Rightarrow \boxed{\frac{m}{k} \frac{d^2 s}{dt^2} + \frac{c}{k} \frac{ds}{dt} + s = L_0}$$



List of standard ODEs for vibration problems

Case I $\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + x = C$

Case II $\frac{1}{\alpha^2} \frac{d^2 x}{dt^2} - x = -C$

Case III $\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dx}{dt} + x = C$

Case IV $\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dx}{dt} + x = C + KF(t)$ with $F(t) = F_0 \sin \omega t$

Case V $\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dx}{dt} + x = C + K \left(y + \frac{2\zeta}{\omega_n} \frac{dy}{dt} \right)$ with $y(t) = Y_0 \sin \omega t$

Case VI $\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dx}{dt} + x = C - \frac{K}{\omega_n^2} \frac{d^2 y}{dt^2}$ with $y(t) = Y_0 \sin \omega t$

Case VII $\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dx}{dt} + x = K \left(\frac{\lambda^2}{\omega_n^2} \frac{d^2 y}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dy}{dt} + y \right)$ with $y(t) = Y_0 \sin \omega t$

Our eq: $\frac{m}{k} \frac{d^2 s}{dt^2} + \frac{c}{k} \frac{ds}{dt} + s = L_0$

$\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dx}{dt} + x = C$

$x \equiv s$

$C \equiv L_0$

$\frac{1}{\omega_n^2} \equiv \frac{m}{k}$

$\omega_n^2 \equiv \frac{k}{m}$

$\frac{2\zeta}{\omega_n} \equiv \frac{c}{k}$

$\omega_n = \sqrt{\frac{k}{m}}$

$\zeta = \frac{c}{2\sqrt{km}}$

"Damping Coefficient"

Solution to Case III (From pdf on website)

Solution to $\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dx}{dt} + x = C$ with $x = x_0$ $\frac{dx}{dt} = v_0$ $t = 0$

Let $\omega_d = \omega_n \sqrt{|1 - \zeta^2|}$ (Note absolute value)

Overdamped $\zeta > 1$ $x(t) = C + \exp(-\zeta\omega_n t) \left\{ \frac{v_0 + (\zeta\omega_n + \omega_d)(x_0 - C)}{2\omega_d} \exp(\omega_d t) - \frac{v_0 + (\zeta\omega_n - \omega_d)(x_0 - C)}{2\omega_d} \exp(-\omega_d t) \right\}$

Critically Damped $\zeta = 1$ $x(t) = C + \{(x_0 - C) + [v_0 + \omega_n(x_0 - C)]t\} \exp(-\omega_n t)$

Underdamped $\zeta < 1$ $x(t) = C + \exp(-\zeta\omega_n t) \left\{ (x_0 - C) \cos \omega_d t + \frac{v_0 + \zeta\omega_n(x_0 - C)}{\omega_d} \sin \omega_d t \right\}$

Recall $\omega_n = \sqrt{\frac{k}{m}}$

$\zeta = \frac{c}{2\sqrt{km}}$

Underdamped Solution ($\zeta < 1$)

$$x(t) = A \exp(-\zeta \omega_n t) \sin(\omega_d t + \phi)$$

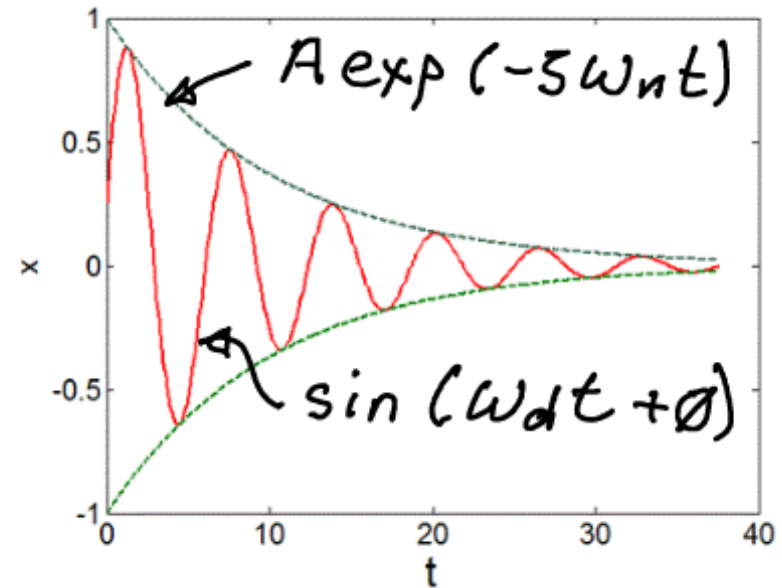
$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

Notes:

- (1) Exponentially decaying vibrations
- (2) Frequency ω_d (slightly smaller than ω_n)
- (3) Decays as $\exp(-\zeta \omega_n t)$

Vibrations decay faster as $\zeta \rightarrow 1$

Fastest decay for $\zeta = 1$ - Critical Damping



Overdamped Solution $\zeta > 1$

$$x(t) = \exp(-\zeta \omega_n t) \{ A \exp(\omega_d t) + B \exp(-\omega_d t) \}$$

$$\omega_d = \omega_n \sqrt{\zeta^2 - 1}$$

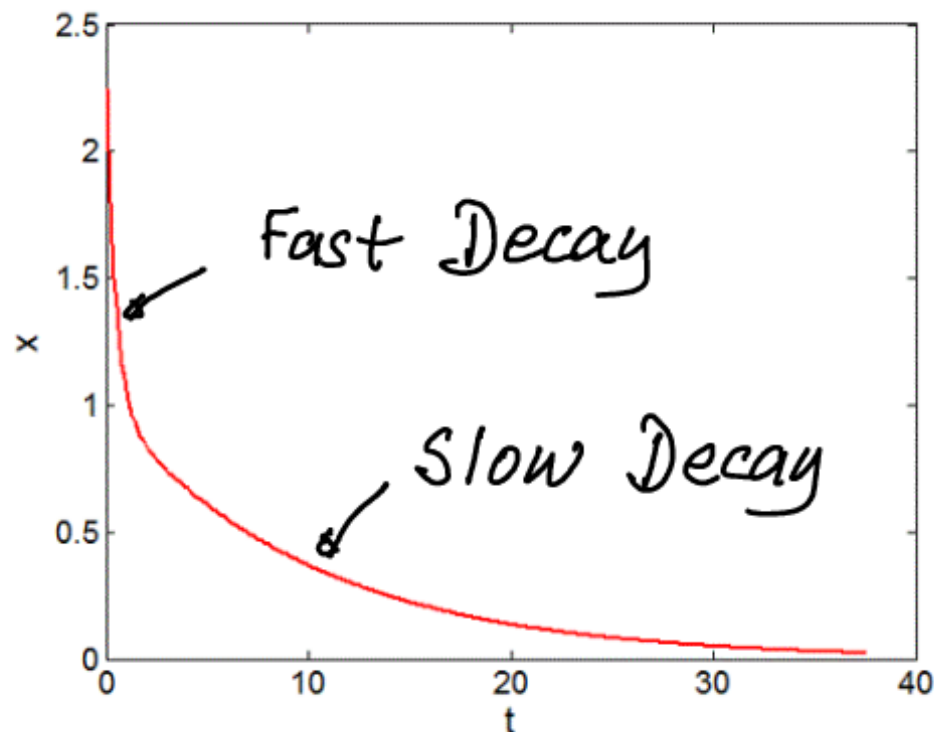
$$\Rightarrow x(t) = A \exp \left\{ -\omega_n t (\zeta - \sqrt{\zeta^2 - 1}) \right\} + B \exp \left\{ -\omega_n t (\zeta + \sqrt{\zeta^2 - 1}) \right\}$$

Decays slowly
Decays quickly

Notes:

- (1) No vibrations
- (2) Slowest term decays faster as $\zeta \rightarrow 1$
slower as $\zeta \rightarrow \infty$

Fastest decay for $\zeta = 1$



Engineering Implications

(1) To stop vibrations $\zeta \geq 1 \Rightarrow c \geq 2\sqrt{km}$

(2) For fastest return to equilibrium

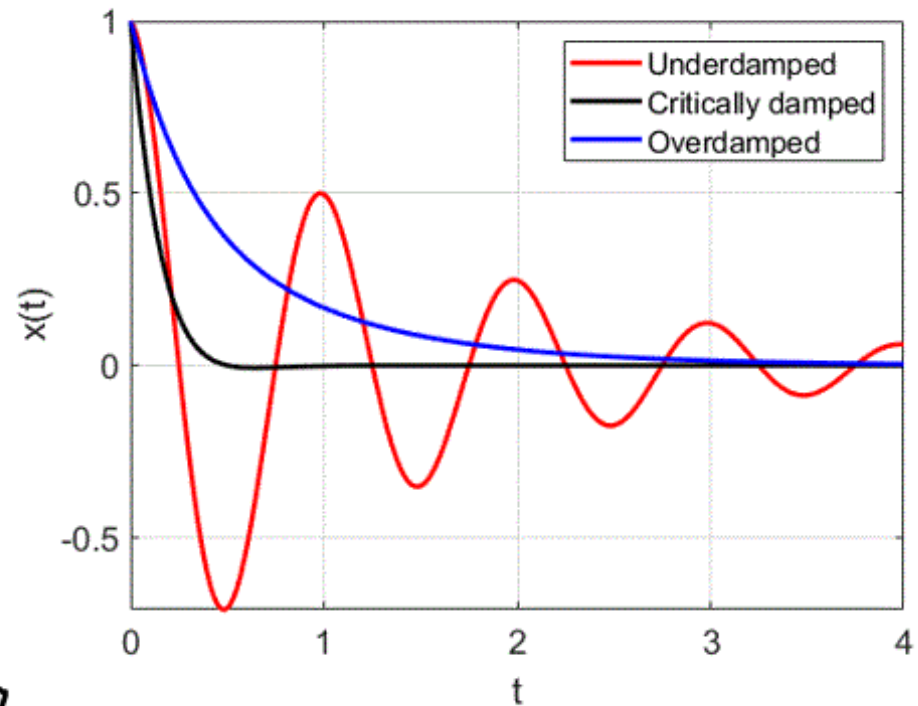
(a) Choose critical damping $\zeta = 1$

Then $x \approx A \exp(-\omega_n t)$

Hence maximize ω_n

$\Rightarrow$ maximize $\omega_n = \sqrt{\frac{k}{m}}$

Choose $c = 2\sqrt{km}$

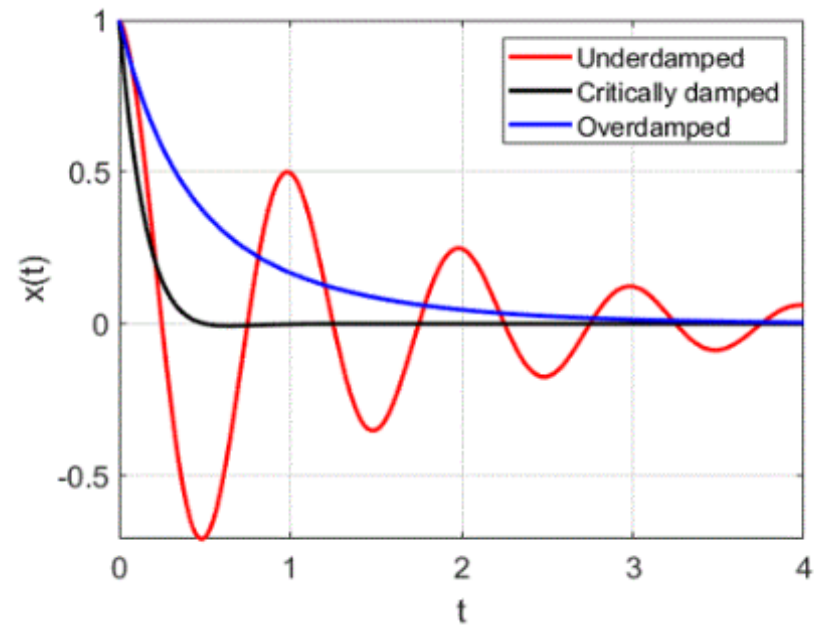


Underdamped System

Amplitude decays as $\exp(-\zeta \omega_n t)$

$\Rightarrow$ increase $\zeta \omega_n = c/(2m)$

$\Rightarrow$ increase c or reduce m



Overdamped System

x decays as $\exp\{-\omega_n (\zeta - \sqrt{\zeta^2 - 1}) t\}$
 $\approx \exp\{-\omega_n t / (2\zeta)\}$ for $\zeta \gg 1$

$\Rightarrow$ increase $\omega_n / (2\zeta) = k / (2c)$

$\Rightarrow$ increase k or reduce c

Solving the case III vibration equation

Background: Complex Variables

Define $i = \sqrt{-1}$ General complex number $z = a + ib$

Complex conjugate $\bar{z} = a - ib$  $a = (z + \bar{z}) / 2$ $b = -i(z - \bar{z}) / 2$

Euler's formula $e^{i\theta} = \cos \theta + i \sin \theta$

 Polar / rectangular conversion

 Trig functions

$$a + ib = \rho e^{i\theta} \quad \rho = \sqrt{a^2 + b^2} \quad \theta = \tan^{-1}(b / a)$$

$$a = \rho \cos \theta \quad b = \rho \sin \theta$$

$$\cos \theta = (e^{i\theta} + e^{-i\theta}) / 2$$

$$\sin \theta = -i(e^{i\theta} - e^{-i\theta}) / 2$$

Calculus

$$\frac{de^{i\omega t}}{dt} = i\omega e^{i\omega t} \qquad \frac{d^2 e^{i\omega t}}{dt^2} = -\omega^2 e^{i\omega t}$$

Solving the case III vibration equation

Solve: $\frac{1}{\omega_n^2} \frac{d^2 x}{dt^2} + \frac{2\zeta}{\omega_n} \frac{dx}{dt} + x = C$ $x = x_0$ $\frac{dx}{dt} = v_0$ $t = 0$

Guess $x = Ae^{\lambda t} + C \rightarrow \left(\frac{\lambda^2}{\omega_n^2} + \frac{2\zeta\lambda}{\omega_n} + 1 \right) Ae^{\lambda t} = 0$ (characteristic equation)

Roots $\lambda = -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$

$\zeta > 1$ (Overdamped) $\Rightarrow$ two real roots

$$\lambda = -\zeta\omega_n \pm \omega_d$$

$\zeta = 1$ (Critically damped) $\Rightarrow$ one real root

$$\lambda = -\omega_n$$

$\zeta < 1$ (Underdamped) $\Rightarrow$ two complex roots

$$\lambda = -\zeta\omega_n \pm i\omega_d$$

$$\omega_d = \sqrt{\zeta^2 - 1}$$

Note absolute value

General Solution:

$$\zeta > 1 \Rightarrow x = C + A_1 e^{(-\zeta\omega_n + \omega_d)t} + A_2 e^{(-\zeta\omega_n - \omega_d)t}$$

$$\zeta = 1 \Rightarrow x = C + A_1 e^{-\zeta\omega_n t} + A_2 t e^{-\zeta\omega_n t}$$

$$\zeta < 1 \Rightarrow x = C + A_1 e^{(-\zeta\omega_n + i\omega_d)t} + A_2 e^{(-\zeta\omega_n - i\omega_d)t}$$

A_1, A_2 Determined by initial conditions

Solving the case III vibration equation

Overdamped Solution: $\zeta > 1 \Rightarrow x = C + A_1 e^{(-\zeta\omega_n + \omega_d)t} + A_2 e^{(-\zeta\omega_n - \omega_d)t}$

Initial Conditions: $x(0) = C + A_1 + A_2 = x_0$

$$\left. \frac{dx}{dt} \right|_{t=0} = A_1(\omega_d - \zeta\omega_n) - A_2(\omega_d + \zeta\omega_n) = v_0$$

$$\Rightarrow A_1 = \frac{v_0 + (\zeta\omega_n + \omega_d)(x_0 - C)}{2\omega_d} \quad A_2 = -\frac{v_0 + (\zeta\omega_n - \omega_d)(x_0 - C)}{2\omega_d}$$

$$x(t) = C + \exp(-\zeta\omega_n t) \left\{ \frac{v_0 + (\zeta\omega_n + \omega_d)(x_0 - C)}{2\omega_d} \exp(\omega_d t) - \frac{v_0 + (\zeta\omega_n - \omega_d)(x_0 - C)}{2\omega_d} \exp(-\omega_d t) \right\}$$

Solving the case III vibration equation

Critically Damped Solution: $\zeta = 1 \Rightarrow x = C + A_1 e^{-\zeta \omega_n t} + A_2 t e^{-\zeta \omega_n t}$

Initial Conditions: $x(0) = C + A_1 = x_0$

$$\left. \frac{dx}{dt} \right|_{t=0} = -\omega_n A_1 + A_2 = v_0$$

$$A_1 = x_0 - C \quad A_2 = v_0 + \omega_n (x_0 - C)$$

$$x(t) = C + \{(x_0 - C) + [v_0 + \omega_n (x_0 - C)]t\} \exp(-\omega_n t)$$

Solving the case III vibration equation

Underdamped Solution: $\zeta < 1 \Rightarrow x = C + A_1 e^{(-\zeta\omega_n + i\omega_d)t} + A_2 e^{(-\zeta\omega_n - i\omega_d)t}$

Initial Conditions: $x(0) = C + A_1 + A_2 = x_0$

$$\left. \frac{dx}{dt} \right|_{t=0} = A_1(i\omega_d - \zeta\omega_n) - A_2(i\omega_d + \zeta\omega_n) = v_0$$

$$\Rightarrow A_1 = -i \frac{v_0 + (\zeta\omega_n + i\omega_d)(x_0 - C)}{2\omega_d} \quad A_2 = i \frac{v_0 + (\zeta\omega_n - i\omega_d)(x_0 - C)}{2\omega_d}$$

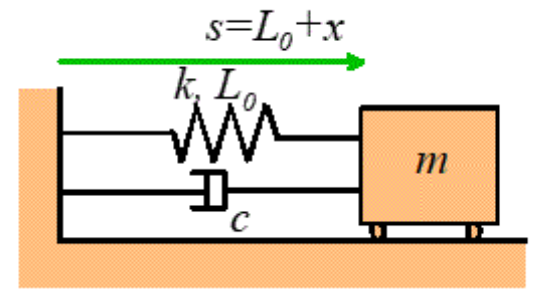
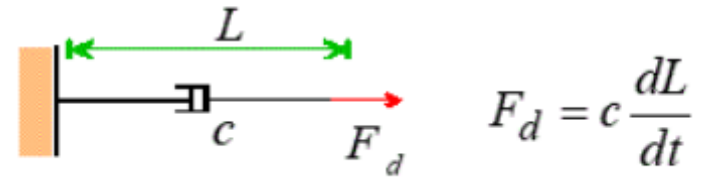
$$x(t) = C + \exp(-\zeta\omega_n t) \left\{ (x_0 - C) \frac{1}{2} (e^{i\omega_d t} + e^{-i\omega_d t}) - \frac{v_0 + \zeta\omega_n(x_0 - C)}{\omega_d} \frac{i}{2} (e^{i\omega_d t} - e^{-i\omega_d t}) \right\}$$

Euler's formula:

$$x(t) = C + \exp(-\zeta\omega_n t) \left\{ (x_0 - C) \cos \omega_d t + \frac{v_0 + \zeta\omega_n(x_0 - C)}{\omega_d} \sin \omega_d t \right\}$$

5.5.3 Summary of constants used in damped vibration formulas

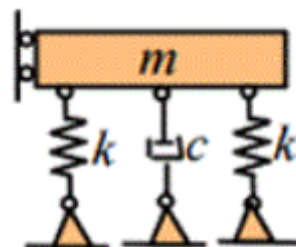
- (1) The constant c (called "dashpot coefficient" or "damping coefficient")
- (2) ω_n : "Un-damped natural frequency" $\omega_n = \sqrt{k/m}$
- (3) ζ : called "damping coefficient" or "damping ratio" $\zeta = c / (2\sqrt{km})$
Some texts call the product $\zeta \omega_n$ the "damping ratio"
- (4) ω_d : "Damped natural frequency"
 $\omega_d = \omega_n \sqrt{1 - \zeta^2}$



Terminology can be confusing !

5.5.4: Example: The spring-mass system shown in the figure is critically damped.

Find the new damping factor if one spring is removed.



Formula $\zeta = c / (2 \sqrt{km})$
"Critical damping" $\Rightarrow \zeta = 1$

For original system $\zeta_1 = \frac{c}{2 \sqrt{2km}} = 1$

For system with 1 spring removed

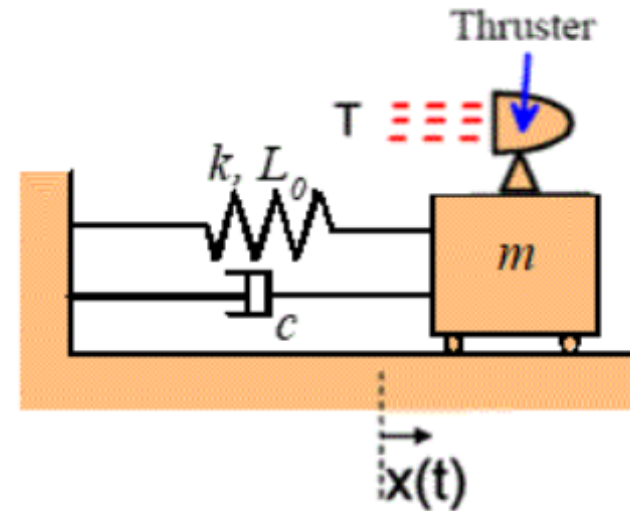
$$\zeta_2 = \frac{c}{2 \sqrt{km}} = \sqrt{2} \zeta_1 = \sqrt{2}$$

5.5.5 Example: Design a thrust-stand

Constraints:

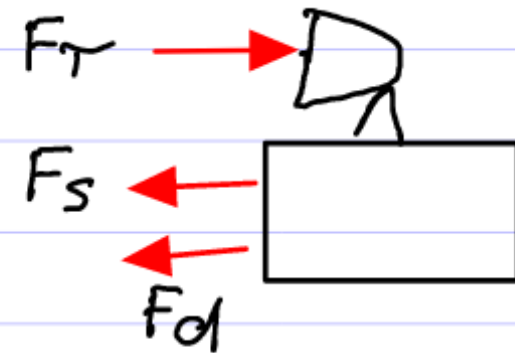
1. Mass of stand+engine 1000kg
2. Max expected thrust: 100 kN
3. Max deflection 1cm
4. Must reach equilibrium deflection as quickly as possible

Find values for k and c .



Approach: (1) Statics to find k
(2) Critical damping to find c

(1) Statics



$$\sum F = 0 \Rightarrow F_T - F_S - F_d = 0$$

$$F_S = kx$$

$$F_d = c \frac{dx}{dt} = 0 \text{ because static}$$

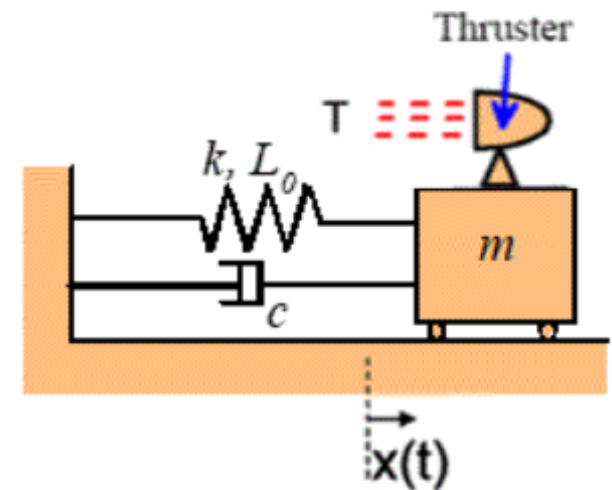
Hence $F_T = kx \Rightarrow k = F_T/x = 10^7 \text{ N/m}$

5.5.5 Example: Design a thrust-stand

Constraints:

1. Mass of stand+engine 1000kg
2. Max expected thrust: 100 kN
3. Max deflection 1cm
4. Must reach equilibrium deflection as quickly as possible

Find values for k and c .



$$\text{Critical damping} \Rightarrow \zeta = \frac{c}{2\sqrt{km}} = 1$$

$$\Rightarrow c = 2\sqrt{km} = 200 \text{ kNs/m}$$

5.5.6: Example: Impact of a baseball is idealized as a damped spring-mass system.

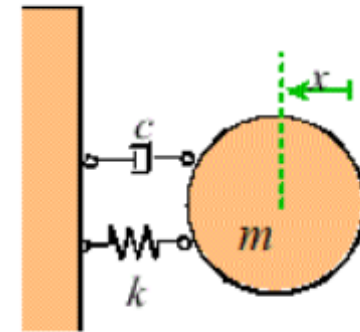
At time $t=0$ $x=0$, $\frac{dx}{dt} = v_0$

Find a formula for $x(t)$ in terms of ζ, ω_n

If ζ is small, rebound occurs at approximately $x=0$

Show that the restitution coefficient is $e \approx \exp(-\pi\zeta)$

The impact movie shows contact last for 4 millisecc and $e=0.6$. The baseball has mass 0.145kg. Find k, c for the baseball



Approach (1) Derive EOM ($\underline{F} = m\underline{a}$)

(2) Solve

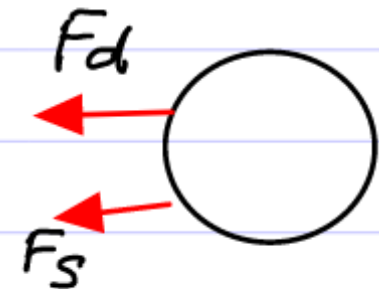
(3) Use solution to predict rebound velocity $\Rightarrow$ find e

$$\underline{F} = m\underline{a}$$

$$m \frac{d^2x}{dt^2} = F_s + F_d$$

$$F_s = -kx$$

$$F_d = -c \frac{dx}{dt}$$



$$\Rightarrow m \frac{d^2x}{dt^2} + c \frac{dx}{dt} + kx = 0$$

Hence $\frac{1}{\omega_n^2} \left(\frac{m}{k} \right) \frac{d^2x}{dt^2} + \left(\frac{c}{k} \right) \frac{dx}{dt} + x = 0$
 ω_n^2 $2.5/\omega_n$

Case III EOM with $\omega_n = \sqrt{\frac{k}{m}}$ $\zeta = \frac{c}{2\sqrt{km}}$

We know ball rebounds $\Rightarrow$ underdamped
 $\Rightarrow \zeta < 1$

$$x(t) = C + \exp(-\zeta\omega_n t) \left\{ (x_0 - C) \cos \omega_d t + \frac{v_0 + \zeta\omega_n(x_0 - C)}{\omega_d} \sin \omega_d t \right\}$$

$$C = 0$$

Given $x = 0$ @ $t = 0 \Rightarrow x_0 = 0$
 $dx/dt = v_0$ @ $t = 0$

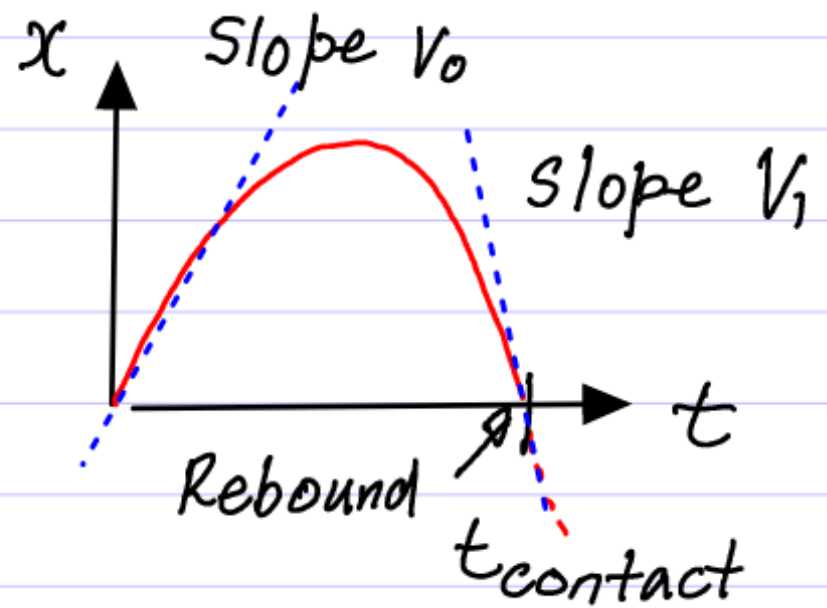
$$\Rightarrow x(t) = \frac{v_0}{\omega_d} \exp(-\zeta\omega_n t) \sin \omega_d t$$

$$\omega_d = \omega_n \sqrt{1 - \zeta^2}$$

Understanding Solution

Restitution coefficient

$$e = -\frac{v_1}{v_0}$$



At rebound $x \sim 0$

$$\Rightarrow \sin(\omega_d t_{\text{contact}}) = 0$$

$$\Rightarrow \omega_d t_{\text{contact}} = \pi$$

$$\Rightarrow t_{\text{contact}} = \pi / \omega_d$$

$$\begin{aligned} v &= \frac{dx}{dt} = \frac{d}{dt} \left\{ \frac{v_0}{\omega_d} \exp(-\zeta \omega_n t) \sin \omega_d t \right\} \\ &= \frac{v_0}{\omega_d} \exp(-\zeta \omega_n t) \left\{ -\zeta \omega_n \sin \omega_d t + \omega_d \cos \omega_d t \right\} \end{aligned}$$

Rebound Velocity : substitute $t = \pi/\omega_d$

$$\Rightarrow v_1 = -\frac{v_0}{\omega_d} \exp\left(-\frac{3\omega_n \pi}{\omega_d}\right) \omega_d$$

$$\text{Hence } e = \frac{-v_1}{v_0} = \exp\left(-\frac{3\omega_n \pi}{\omega_d}\right)$$

$\omega_n \sqrt{1-\zeta^2}$

Note for $\zeta \ll 1$ $\sqrt{1-\zeta^2} \approx 1$

$$\text{Hence } e = \exp(-\pi \zeta)$$

Finally find k, c from given data

$$(1) e = 0.6 \Rightarrow \exp(-\pi \zeta) = 0.6 \Rightarrow \zeta = \frac{-1}{\pi} \log(0.6)$$

$$\Rightarrow \zeta = 0.16$$

$$(2) t_{\text{contact}} = 4 \times 10^{-3} \text{ s} \quad t_{\text{contact}} = \frac{\pi}{\omega_d}$$

$$\Rightarrow \omega_n = \frac{\pi}{t_{\text{contact}} \sqrt{1-\zeta^2}} = 7900 \text{ rad/s}$$

$$\omega_n = \sqrt{\frac{k}{m}} \Rightarrow k = m \omega_n^2 \quad m = 0.145 \text{ kg}$$

$$\Rightarrow k = 1.14 \text{ kN/m}$$

$$\zeta = \frac{c}{2\sqrt{km}} \Rightarrow c = 2\sqrt{km} \zeta = 4.2 \text{ Ns/m}$$

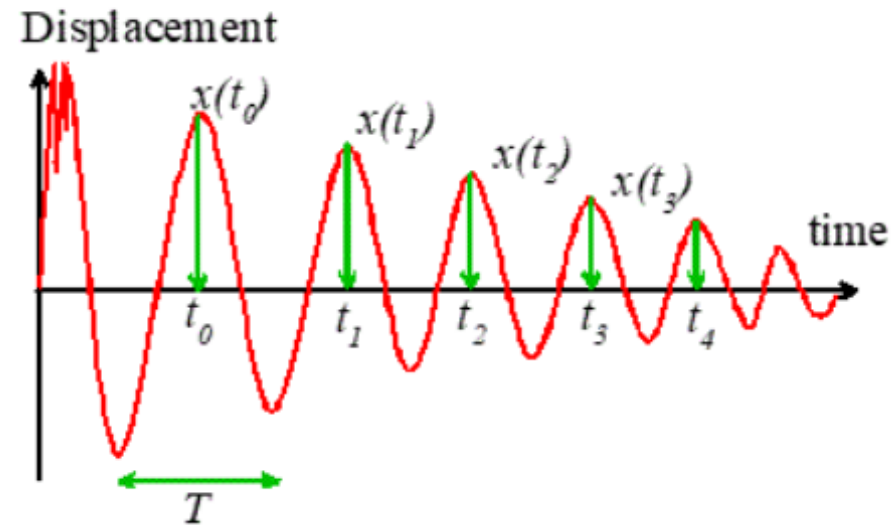
5.5.7 Measuring ω_n and ζ from an impulse test

Impulse test produces a damped vibration response

Procedure

- (1) Find period T
- (2) Find "log decrement"

$$\delta = \frac{1}{n} \underbrace{\log}_{\text{natural log}} \left(\frac{x(t_0)}{x(t_n)} \right)$$



Then

$$\omega_n = \frac{\sqrt{4\pi^2 + \delta^2}}{T}$$

$$\zeta = \frac{\delta}{\sqrt{4\pi^2 + \delta^2}}$$

Proof

Damped vibration sol $x(t) = A \exp(-\zeta \omega_n t) \sin(\omega_d t + \phi)$

$$\text{Hence } \frac{x(t_0)}{x(t_n)} = \frac{\cancel{A \exp(-\zeta \omega_n t_0) \sin(\omega_d t_0 + \phi)}}{\cancel{A \exp\{-\zeta \omega_n (t_0 + nT)\} \sin\{\omega_d (t_0 + nT) + \phi\}}}$$

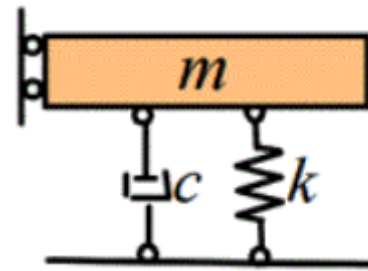
$$\Rightarrow \frac{x(t_0)}{x(t_n)} = \exp(\zeta \omega_n nT)$$

$$\Rightarrow \zeta = \frac{1}{n} \log \left(\frac{x(t_0)}{x(t_n)} \right) = \zeta \omega_n T$$

$$\text{Recall } T = 2\pi / \omega_d \quad \omega_d = \omega_n \sqrt{1 - \zeta^2}$$

$$\Rightarrow \zeta = \frac{2\pi \zeta}{\sqrt{1 - \zeta^2}} \Rightarrow \zeta = \frac{\delta}{\sqrt{4\pi^2 + \delta^2}} \quad \omega_n = \frac{\delta}{3T} = \frac{\sqrt{4\pi^2 + \delta^2}}{T}$$

Example: Fig shows vibration of a vibration isolation table.



Find ω_n, ζ

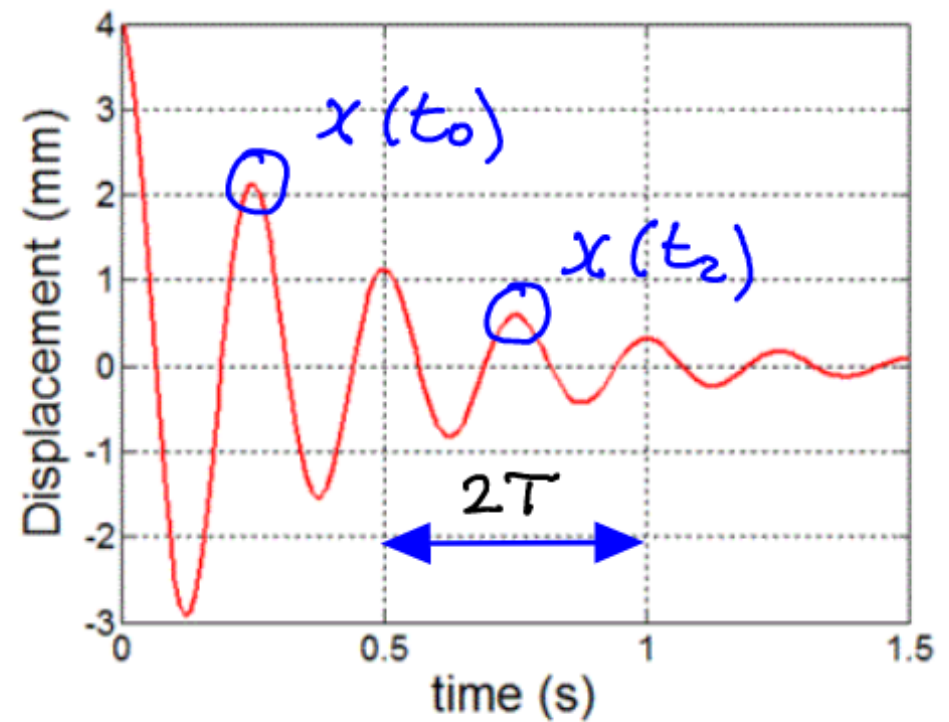
Approach: Use formulas

From graph:

(1) $T = 0.25 \text{ s}$

(2) Log decrement

$$\delta = \frac{1}{2} \log \left(\frac{2.1}{0.6} \right) = 0.63$$



$$\zeta = \frac{\delta}{\sqrt{4\pi^2 + \delta^2}} = 0.1$$

$$\omega_n = \frac{\sqrt{4\pi^2 + \delta^2}}{T} \approx 25 \text{ rad/s}$$